PRINT DATE: 04/01/92

FAILURE MODES EFFECTS ANALYSIS (FMEA) -- CRITICAL HARDHARE

NUMBER: M4-18G-RY030-X

SUBSYSTEM NAME: ELECTRICAL POWER GENERATION - CRYO, GENERIC

REVISION: 1 11/12/91

PART NAME VENDOR NAME

PART HUMBER VENDOR NUMBER

≡ SRU :

RELIEF VALVE, H2 TANK

PARKER HANNIFIN

MC264-0440-0402

575000Z-102

**EXTENDED DESCRIPTION OF PART UNDER ANALYSIS:** RELIEF VALVE, H2 TANK

REFERENCE DESIGNATORS:

40Y45RV030

40Y45RV040

40V45RV500

40V45RV560

40V45RV660

40V45RV862

40V45RV872

40V45RV882

40V45RV892

■ QUANTITY OF LIKE ITEMS: 1 ONE PER TANK

■ FUNCTION:

PROVIDES OVERPRESSURIZATION PROTECTION FOR H2 TARKS.

S. Gavit

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FAILURE MODES EFFECTS AMALYSIS (FMEA) -- CRITICAL FAILURE MODE MUMBER: M4-18G-RV030-02

- (8) INTERFACING SUBSYSTEM(S): SAME AS (A)
- (f) MISSION: (A) ZA 3MAZ
- # (D) CREW, VEHICLE, AND ELEMENT(S): SAME AS (A)
- (E) FUNCTIONAL CRITICALITY EFFECTS:

  POSSIBLE LOSS OF CREM/VEHICLE DUE TO TANK RUPTURE IF AN ADDITIONAL FAILURE RESULTS IN TANK OVERPRESSURIZATION.

## - DISPOSITION RATIONALE -

- A) DESIGN:

  15 MICRON FILTER INCORPORATED IN INLET OF RELIEF VALVE. CRYO PLUMBING CLEANED TO LEVEL 200 BY PARTICULATE COUNT. ALL COMPONENTS ARE COMPATIBLE WITH WORKING FLUIDS. VALVE IS MOUNTED WITH BODY AXIS PERFENDICULAR TO VEHICLE X-AXIS TO MINIMIZE VIBRATION EFFECTS. BUILT IN THERMAL COMPENSATION BY THE USE OF BELLEVILLE SPRINGS. VALVE IS CONSTRUCTED OF CRES METALS, CARBON COMPOSITION (VESPEL), AND 6061-T651 ALUMINUM WHICH IS NOT IN CONTACT WITH THE WORKING FLUID.
- OUALIFICATION TESTS INCLUDED; MECHANICAL SHOCK (20 G), SINUSOIDAL VIBRATION (+/- 0.25 G PEAK), RANDOM VIBRATION (0.05 G SQ/HZ MAXIMUM FOR 48 MINUTES). OPERATING CYCLES (1500 AT AMBIENT AND 1400 AT LHZ TEMP), AND THERMALLY CYCLED 5 TIMES (START INITIALLY AT +220 DEG F AND FLOW UNTIL INLET TEMP DROPS TO -380 DEG F).

ACCEPTANCE INCLUDES FUNCTIONAL TEST WITH THERMAL CYCLES (AMBIENT TO +220 DEG F TO AMBIENT TO -300 DEG F TO AMBIENT). VALVE IS FURTHER FUNCTIONALLY VERIFIED DURING PANEL MODULAR ASSEMBLY AND SUBSYSTEM CHECKOUT.

- OMRSD: RELIEF VALVE CRACK AND RESEAT TEST PERFORMED DURING EVERY CRBITER MAINTENANCE DOWN PERIOD (OMDP) OR IF VALVE OPERATED DURING THE PREVIOUS FLIGHT OR TURNAROUND.
- (C) INSPECTION:
   RECEIVING INSPECTION
   TEST REPORTS AND MATERIALS CERTIFICATIONS ARE MAINTAINED CERTIFYING MATERIALS AND PHYSICAL PROPERTIES.

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CONTAMINATION CONTROL CLEANLINESS PER SPECIFICATION TO LEVEL 2004 IS VERIFIED BY INSPECTION.

ASSEMBLY/INSTALLATION :
ALL PARTS ARE PROTECTED FROM DAMAGE AND CONTAMINATION. DIMENSIONAL AND SURFACE FINISH ARE VERIFIED. ALL SURFACES REQUIRING CORROSION PROTECTION ARE CERTIFIED. MANDATORY INSPECTION POINTS ARE INCLUDED IN THE ASSEMBLY PROCEDURE.

CRITICAL PROCESSES
PASSIVATION AND APPLICATION OF BRAYCOTE LUBE IS VERIFIED BY INSPECTION.

NONDESTRUCTIVE EVALUATION ALL INTERNAL WELDS ARE VERIFIED BY THE FOLLOWING INSPECTIONS: 4X VISUAL, DIMENSIONAL, DYE PENETRANT, AND RADIOGRAPHIC EXAMINATION.

TESTING
PROOF PRESSURE TESTING DURING ATP VERIFIES STRUCTURAL INTEGRITY OF THE VALVE AND IS VERIFIED BY INSPECTION.

HANDLING/PACKAGING
PACKAGING FOR SHIPMENT IS VERIFIED BY INSPECTION.

O) FAILURE HISTORY: CAR NO. A7286-010 DOWNEY, RELIEF PANEL ATP IN HZ TINK RELIEF VALVE FAILED TO CRACK WITHIN SPECIFICATION DURING THE LOW TEMPERATURE TEST OF THE ACCEPTANCE TEST. THE ANALYSIS DETERMINED THE FAILURE TO BE CAUSED BY THE TEST SETUP, NOT THE VALVE. THE UNIT FAILED DUE TO EXCESS MOISTURE WITHIN THE TEST SETUP WHICH CAUSED ICING AND BLOCKAGE OF THE PILOT SECTION OF THE VALVE.

CORRECTIVE ACTION INCLUDED REVISING THE TEST SETUP AND TEST PROCEDURES TO ELIMINATE EXCESS MOISTURE WITHIN THE SYSTEM.

CAR NO. AD3231-010 DOWNEY, MISSION SIMULATION PALLET ATP
AN H2 RELIEF VALVE EXHIBITED OUT OF SPECIFICATION LEAKAGE UPON RESEAT
DURING DOWNEY MISSION SIMULATION PALLET PANEL ACCEPTANCE TESTING.
FAILURE OF THE VALVE TO RESEAT WAS DUE TO THE PUSHROO ACTUATING THE
MAIN RELIEF VALVE POPPET BOUND WITHIN THE UPPER HOUSING BORE. PUSH ROD
BINDING IS SUSPECTED TO HAVE BEEN CAUSED BY A CONTAMINANT. THIS
CAMAGED THE BUSHING/PUSHROD BORE SLIDING SURFACES TO THE POINT WHERE
THE MAIN SPRING COULD NOT OVERCOME THE INCREASED FRICTIONAL FORCES.
THE SOURCE OF CONTAMINANT COULD NOT BE DETERMINED.
THE PROBLEM WAS CLOSED WITH THE FOLLOWING RATIONALE: THE RELIEF VALVE
PERFORMED ITS PRIMARY FUNCTION WHICH IS CRACKING AT 302 PSIG AND—STAYED
OPEN TO PREVENT A SYSTEM OVERPRESSURIZATION CONDITION. ANALYSIS HAS
INDICATED A LOAD OF 500 POUNDS ON THE PUSHROD ASSEMBLY DURING NORMAL

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FAILURE MODES EFFECTS AMALYSIS (FMEA) -- CRITICAL FAILURE MODE
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FLOW CONDITIONS ACTING AGAINST A 26 POUND LOAD WHICH IS COMPRISED OF: THE SPRING LOAD, BUSHING FRICTION, AND THE INLET PRESSURE. THIS IS THE FIRST REPORTED FAILURE OF AN HZ RELIEF VALVE FAILING RESEAT DUE TO A STUCK POPPET PUSH ROO. SINCE ALL RELIEF VALVES ARE VERIFIED TO BE CLOSED PRIOR TO TLAUNCH, A PRIOR NON RELATED SYSTEM FAILURE WOULD BE REQUIRED BEFORE THE RELIEF VALVE WOULD BE NEEDED TO RELIEVE. ALSO, TO REDUCE THE PROBABILITY OF THIS PROBLEM FROM RECURRING ON FUTURE HARDWARE ALL RELATED PARTS HAVE BEEN REMOVED FROM STOCK FOR INSPECTION OF OUT OF SPECIFICATION CONDITIONS. A REQUIREMENT WAS ACCED TO INSPECT THE BUSHINGS AT 10X MAGNIFICATION AND THE 8 MICRON SURFACE FIXISH OF THE ASSEMBLY PUSHEDO BORE ARE NOW VERIFIED WITH A BORDSCOPE.

© (E) OPERATIONAL USE: CREW WILL RESPOND TO TANK OVERPRESSURE ANNUNCIATION BY DEACTIVATING AFFECTED TANK HEATERS.

## - APPROVALS -

RELIABILITY ENGINEERING: M. D. WEST DESIGN ENGINEERING : M. M. SCHEIERN DUALITY MANAGER : D. J. BUTTHER HASA RELIABILITY :

YASA SUBSYSTEM MANAGER : NASA QUALITY ASSURANCE : m Kt Anderger